CLAIMS

- 1. A method for selecting a maximum size for catalyst particles used in a multiphase reactor, wherein the multiphase reactor includes a liquid and a catalyst at conversion promoting conditions, said liquid having a density, ρ_L , and viscosity, μ_L , under said conversion promoting conditions and said catalyst comprising particles with a particle density, ρ_P , and particle sizes, d_P , the method comprising the steps of:
 - (a) selecting a catalyst non-uniformity in the multiphase reactor;
 - (b) determining an Archimedes number, Ar, corresponding to said catalyst non-uniformity; and
 - (c) calculating a maximum catalyst diameter from said Archimedes number, Ar, according to the equation $d_P = \sqrt[3]{\frac{Ar\mu_L^2}{g\rho_L(\rho_P \rho_L)}}$.
- 2. The method of claim 1 wherein the catalyst and conversion promoting conditions promote Fischer-Tropsch synthesis.
- 3. The method of claim 1 wherein the multiphase reactor comprises a slurry bubble column reactor.
- 4. The method of claim 1, wherein the catalyst non-uniformity is less than about 3, and the maximum catalyst diameter is equal to or less than about 250 microns.
- 5. The method of claim 1, further comprising the step of:
 - (d) selecting a minimum catalyst diameter based on a minimum particle settling velocity, a filter permeability, or a combination thereof.
- 6. The method of claim 5, wherein the minimum catalyst diameter is equal to or greater than about 10 microns.
- 7. A method for determining an optimum catalyst particle distribution for use in a synthesis process comprising a separation system and a slurry bubble reactor, wherein the slurry bubble

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reactor contains a liquid and a catalyst at conversion promoting conditions, wherein the liquid has a density, ρ_L , and viscosity, μ_L , under said conversion promoting conditions, and wherein the catalyst comprises particles having a particle density, ρ_P , and particle size, d_P , the method comprising the steps of:

- (a) calculating a maximum catalyst particle size comprising the steps of:
 - (1) choosing a catalyst non-uniformity in the slurry bubble reactor;
 - (2) finding an Archimedes number, Ar, appropriate to the catalyst non-uniformity; and
 - (3) calculating the maximum catalyst particle size based on the Archimedes number according to the equation $d_P = \sqrt[3]{\frac{Ar\mu_L^2}{g\rho_L(\rho_P \rho_L)}}$; and
- (b) calculating a minimum particle size based on a separation property.
- 8. The method of claim 7, wherein the catalyst and the conversion promoting conditions are selected to promote Fischer-Tropsch synthesis.
- 9. The method of claim 7, wherein the separation system comprises at least one unit selected from the group consisting of sedimentation and filtration.
- 10. The method of claim 7, wherein the separation property is selected from the group consisting of catalyst particle terminal velocity, filter permeability, and combinations thereof.
- 11. A method for producing hydrocarbons from synthesis gas in a slurry bubble reactor, the slurry bubble reactor including a liquid and a catalyst at conversion promoting conditions, wherein the liquid has a density, ρ_L , and viscosity, μ_L , under said conversion promoting conditions and wherein the catalyst comprises a plurality of catalyst particles including fresh catalyst particles, the fresh catalyst particles having a particle density, ρ_P , and particle sizes, d_P , the method comprising the steps of:
 - (a) selecting the fresh catalyst particles such that the fresh catalyst particles have Archimedes numbers between about 0.02 and about 250, the Archimedes numbers being defined by $Ar = gd_P^3 \rho_L (\rho_P \rho_L)/\mu_L^2$; and

- (b) passing a synthesis gas feed stream in said slurry bubble reactor over said catalyst under said conversion promoting conditions to convert at least a portion of said synthesis gas feed stream to hydrocarbons.
- 12. The method of claim 11, wherein a majority of said catalyst particles have particle sizes between about 10 and about 250 microns.
- 13. The method of claim 12, wherein the catalyst has an effectiveness factor in step (b) greater than about 0.7.
- 14. The method of claim 12, wherein the catalyst particles have an average Reynolds number of less than about 0.1, according to the equation $\operatorname{Re}_{avg} = \sum_{i=1}^{M} f_i \operatorname{Re}_i$, where f_i is the portion of particles in particle size fraction i, which is determined by dividing the number of particles in size fraction i by the total number of particles, which is N, and Re_i is the Reynolds number of particles of size fraction i.
- 15. The method of claim 11, wherein the fresh catalyst particles have Archimedes numbers between about 0.02 and about 100.
- 16. The method of claim 11, wherein the fresh catalyst particles have Archimedes numbers between about 0.2 and about 30.
- 17. The method of claim 11, wherein at least about 90 percent by weight of the catalyst particles have an Archimedes number between about 0.02 and about 100.
- 18. A process for producing hydrocarbons from synthesis gas in a slurry bubble reactor, the slurry bubble reactor including a liquid and a catalyst at conversion promoting conditions, wherein the liquid has a density, ρ_l , and viscosity, μ_l , under said conversion promoting conditions and wherein the catalyst comprises a plurality of particles with a particle velocity, ν , the method comprising the steps of:
- (a) selecting the catalyst particles such that the catalyst particles have an average Reynolds number of less than about 0.1, according to the equation 23

 $\operatorname{Re}_{avg} = \sum_{i=1}^{M} f_i \operatorname{Re}_i$, wherein f_i is the particle size fraction, which is determined by dividing the number of particles of size fraction i by the total number of particles, and Re_i is the Reynolds number of particles of size fraction i; Re_i being defined according to the equation $\operatorname{Re}_i = \frac{\rho_l v D_i}{\mu_l}$, where D_i is the number average particle size of particles in size fraction i; and

- (b) passing a synthesis gas feed stream in said slurry bubble reactor over said catalyst under said conversion promoting conditions to convert at least a portion of said synthesis gas feed stream to hydrocarbons.
- 19. The process according to claim 18 wherein the number average particle size is between about 20 and about 50 microns.
- 20. The process according to claim 19 wherein the number average particle size is between about 30 and about 40 microns.
- 21. The process according to claim 19, wherein the catalyst has an effectiveness factor in step (b) greater than about 0.7.
- 22. The process according to claim 18 wherein at least 90% of the plurality of particles have sizes between about 20 and about 150 microns.
- 23. The process according to claim 18 wherein the plurality of particles comprise a substantially log normal distribution of volume percent of catalyst particles versus particle sizes.
- 24. The process according to claim 18 wherein the plurality of particles have an average Reynolds number of between about 0.05 and about 0.06.